




Effect of P microalloying on magnetic properties and structure of FeSiBNbCu nanocrystalline alloy

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ABSTRACT

Phosphorus (P) is a cheap and effective element that inhibits grain growth and improves soft magnetic properties in Fe-based nanocrystalline alloys. However, most alloys usually require high P content, leading to problems such as volatilization and oxidation during production process. In this paper, we study and report new findings regarding the effect of P microalloying on the magnetic properties, microstructure and magnetic domain structure of $\text{Fe}_{77.8}\text{Si}_{10}\text{B}_{9-x}\text{Cu}_{0.6}\text{Nb}_{2.6}\text{P}_x$ ($x = 0$ and 1) nanocrystalline alloys. The substitution of B by 1 at% P has little influence on the crystallization behavior, saturation magnetic flux density (B_s) and permeability (μ) of the alloy, while effectively reduces the coercivity (H_c) in a wide annealing temperature range. The reduced H_c can be attributed to the low magnetocrystalline anisotropy and wide magnetic domains caused by uniform and fine α -Fe(Si) grains. The mechanism of structural evolution induced by 1 at% P is also been discussed. The P microalloyed nanocrystalline alloy with high B_s of 1.43 T, high μ up to 27,000 at 1 kHz, and low H_c of 1.4 A/m is suitable for magnetic shielding piece of wireless charging.

1 Introduction

As consumer electronics industries develop rapidly, there is an increasing need of wireless charging due to their convenient and safe nature [1]. Being one of the key components in wireless charging devices, magnetic shielding pieces can significantly improve charging efficiency by preventing magnetic leakage

and reducing electromagnetic eddy current [2–6]. The previous magnetic shielding pieces are made of ferrites or Fe-based amorphous alloys. Nowadays, Fe-based nanocrystalline alloys, especially FeSiBNbCu (Finemet) system, are the preferred materials for wireless charging of consumer electronics due to their high saturation magnetic flux density (B_s), high permeability (μ) and very low core loss at

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100–200 kHz [7–10]. Unfortunately, the typical FeSiBNbCu alloys currently in commercial use cannot meet the development needs of high charging power and thinning at the same time due to its low B_s (< 1.25 T). Therefore, there is an urgent need to develop nanocrystalline alloys with higher B_s and excellent soft magnetic properties for wireless charging.

Most prior research enhanced B_s by increasing the proportion of ferromagnetic elements (such as Fe, Co, etc.) in the composition [11–13]. However, a high proportion of ferromagnetic elements usually reduces the amorphous forming ability (AFA) of the alloys, thereby worsening the soft magnetic properties such as μ and coercivity (H_c) [14]. In addition, expensive Co not only increases the cost of raw materials but also increases the H_c of the alloys, which is not conducive to commercial applications [15]. The addition of early transition metals (especially Nb, Zr, Hf, Ta and Mo) [16–19] was found to impede grain growth to aid in AFA and good soft magnetic properties but at the expense of B_s . Adding a small amount of post-transition metal such as Al could achieve high μ and high B_s but reduced the AFA [20]. Compared with the early transition metals, P with smaller atomic size has less negative influence on B_s , and can effectively improve the AFA and soft magnetic properties of the amorphous and nanocrystalline alloys with high Fe content, while reducing the cost of raw materials [21–23]. For example, the synergy of P, Nb and Cu in FeSiBNbCuP system can improve the initial crystal number density, inhibit the growth of nanocrystals during annealing, and improve the microstructure and soft magnetic properties of the alloys [24]. Substitution of Nb by P can reduce the primary crystallization temperature and improve the μ of FeSiBNbCuP alloys. However, when P was used to completely replace Nb, the optimum annealing temperature range and soft magnetic properties deteriorate [22]. The suitable substitution of P for Si inhibits the precipitation of α -Fe and improves the thermal stability of FeSiBNbCuP alloys [21]. In FeSiBNbCu alloys with high Fe content, replacing B with P expands the optimal annealing temperature range, increases the grain density of nanocrystals, and obtains good soft magnetic properties [25]. In addition, P instead of B substitution can suppress the preferred surface crystallization of FeSiBNbCuP alloys, but excessive P addition would promote the oxidation of Fe [23]. In order to maintain high AFA and good soft magnetic

properties, the above-mentioned alloys usually contain 3 at% or more of P, since a trace amount of P has less effective in preventing grain growth in these alloys. Alloys with high P content are easy to volatilize during smelting process, and are easily oxidized during heat treatment, making them difficult to scale production [23, 26]. Therefore, it is of great significance to develop low-P nanocrystalline alloys with high AFA and excellent soft magnetic properties; and reveal the mechanism of the influence of P microalloying on the structure and magnetic properties of the alloys.

In this work, we study in detail the effect of P microalloying on the magnetic properties and structure of $\text{Fe}_{77.8}\text{Si}_{10}\text{B}_{9-x}\text{Cu}_{0.6}\text{Nb}_{2.6}\text{P}_x$ ($x = 0$ and 1 at%). We find that substituting 1 at% P for B has little effect on B_s and μ , but enabling the achievement of lower H_c . The superior magnetic properties, i.e. high B_s of 1.43 T, high μ up to 27,000 at 1 kHz, and low H_c of 1.4 A/m, make the alloy a good candidate for wireless charging magnetic shields. Trace P addition can not only improve the soft magnetic performance, but also reduce the processing difficulty, which provides ideas for the industrial application of P-containing nanocrystalline alloys. We explore the evolution of magnetic properties caused by the addition of minor P using transmission electron microscopy (TEM), magneto-optical Kerr microscopy and crystallization dynamics analysis.

2 Materials and methods

2.1 Materials

All the raw material utilized in the present work involved high pure Fe (99.99 mass%), Si (99.99 mass%), B (99.95 mass%), Nb (99.99 mass%), Cu (99.99 mass%) and pre-alloyed Fe_3P (99.99 mass%).

2.2 Procedure

Alloy ingots with a composition of $\text{Fe}_{77.8}\text{Si}_{10}\text{B}_{9-x}\text{Cu}_{0.6}\text{Nb}_{2.6}\text{P}_x$ ($x = 0$ and 1) were prepared by induction-melting for three time under purity argon atmosphere. The ingots were then broken into small pieces and put into a quartz tube for vacuum melting. The ribbons with a thickness of 22 μm and a width about 1.1 mm were produced by a single-roller melt-spinning method with copper roller speed of 45 m/s

in an argon atmosphere. The crystallization temperature of the as-quenched ribbons was evaluated by differential scanning calorimetry (DSC, NETZSCH 404C) at a heating rate of 40 K/min under high purity argon flow. Heat treatment of the as-quenched specimens was carried out with a furnace under a vacuum degree of 5×10^{-3} Pa followed by water quenching. The annealing parameters were at 803–883 K for 30 min.

2.3 Physical characterization

The microstructure of the annealed samples was identified by X-ray diffraction (XRD, Bruker D8 Advance) with Cu-K α radiation and a high-resolution transmission electron microscopy (HRTEM, TF20). The B_s was evaluated through a vibrating sample magnetometer (VSM, Lakeshore 7410) under a maximum applied field of 800 kA/m. The H_c was measured with a DC B-H loop tracer (EXPH-100, Riken Deshi Co., Ltd) under a maximum applied field of 800 A/m. The μ under the frequency range from 1 kHz to 110 MHz was examined by a HP4294A impedance analyzer in a field of 1 A/m. The magnetic domain images were observed by a Magneto-optical Kerr Effect Microscopy using an Evico Magnetics Kerr Microscope (4–873 K/950MT, Germany) in the longitudinal mode. All the measurements were performed at room temperature.

3 Results and discussion

3.1 Thermal properties

The DSC curves of $\text{Fe}_{77.8}\text{Si}_{10}\text{B}_{9-x}\text{Cu}_{0.6}\text{Nb}_{2.6}\text{P}_x$ ($x = 0$ and 1, hereafter labeled as P_0 and P_1 , respectively) are shown in Fig. 1. Both the DSC curves of P_0 and P_1 have two distinct exothermic peaks with the onset temperatures marked as T_{x1} and T_{x2} . The T_{x1} of P_0 and P_1 are 750 and 753 K, and the T_{x2} of P_0 and P_1 are 926 and 927 K, respectively. Therefore, the substitution of B by 1 at% P has little effect on the crystallization behavior of the present alloy system. According to previous studies [11], the optimal annealing temperature for the formation of high-density bcc-Fe(Si) nanocrystalline grains that responsible for excellent soft magnetic properties should be between T_{x1} and T_{x2} .

3.2 Magnetic properties

Figure 2 shows the B_s , μ and H_c of P_0 and P_1 as a function of annealing temperature. It is clear that the 1 at% P addition has little influence on the B_s of the alloy within the error range. The slightly decrease in B_s from about 1.45 T for P_0 to about 1.43 T for P_1 is ascribed to the substitution of B by P that has larger atomic size and mass. Although the μ of P_0 is greater than that of P_1 at 803 K, the μ of P_1 increases with the annealing temperature and reaches the maximum value above 27,000 at 833 K, which is greater than the μ of P_0 . In a wide annealing temperature range, the substitution of 1 at% P for B has no obvious effect on the μ of the alloy, but it can effectively reduce H_c . As shown in Fig. 2, with the increase of annealing temperature, the H_c of P_0 increases from 2.3 to 3.9 A/m, whereas the H_c of P_1 remains around unchanged and can be as low as 1.4 A/m. The low H_c can reduce the hysteresis loss during high-frequency magnetization [11], which is beneficial to improve the efficiency of wireless charging.

3.3 Microstructure analysis

According to Herzer's random anisotropy model [27], H_c is related to the grain size of nanocrystalline alloys. And the reduction of H_c significantly depends on the magneto-crystalline anisotropy, interparticle interaction and size [28]. In order to clarify the influence of trace P addition on the H_c of the alloy, the microstructure and magnetic domain structure were analyzed by XRD, TEM, and magneto-optic

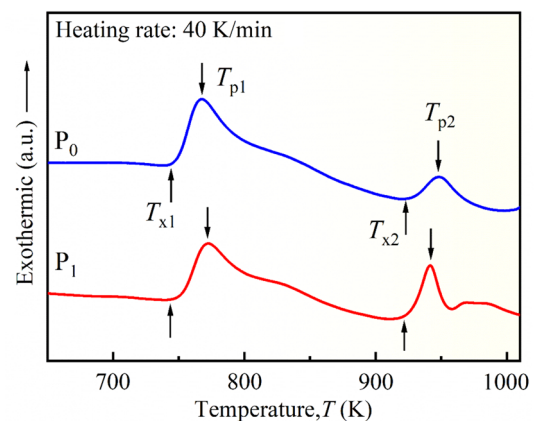


Fig. 1 DSC traces of as-quenched P_0 and P_1 ribbons at a heating rate of 40 K/min. T_{p1} and T_{p2} represent the temperature of the first and second peaks, respectively

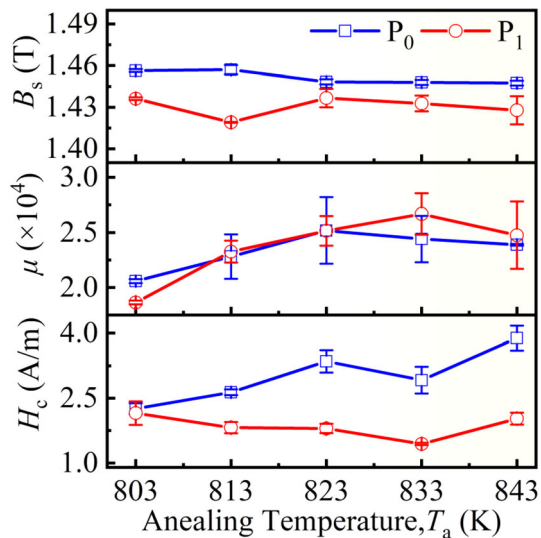


Fig. 2 B_s , μ and H_c of P_0 and P_1 as a function of annealing temperature

Kerr microscope, respectively. Figure 3 displays the XRD patterns of P_0 and P_1 annealed at 803–843 K for 30 min. It is clear that all the samples exhibit one sharp crystalline peak at about $2\theta = 45^\circ$ and two weaker peaks at about $2\theta = 65^\circ$ and 83° , indicating that only α -Fe(Si) single phase is embedded in the residual amorphous matrix [20]. No Fe-boride phase can be observed. With the increase of annealing temperature, the intensity of the crystallization peaks of P_0 and P_1 increases slightly. Figure 4 depicts the TEM micrographs, selected-area electron diffraction (SAED) images and characteristic grain size distribution of P_0 and P_1 annealed at 803 and 843 K. The SAED patterns with a halo pattern and the typical α -Fe(Si) polycrystalline diffraction ring further prove the coexistence of α -Fe(Si) and amorphous phases [29]. The characteristic distribution and average grain sizes D are shown in the histograms. The grain sizes of P_0 and P_1 are almost the same at 803 K, thus their H_c values are similar. The H_c value of P_0 boosts at 843 K, which results from a grain of the average grain size from 11.69 nm at 803 K to 13.85 nm at 843 K and its wider characteristic distribution. However, 1 at% P effectively prevents the growth of α -Fe(Si) at 843 K, thus the grain size and characteristic distribution of P_1 remain basically unchanged as temperature becomes higher. This enables P_1 to maintain low H_c in a wide annealing temperature range.

Figure 5 shows the magnetic domain structure of the as-quenched and annealed P_0 and P_1 . Two kinds of domain structure are observed in the as-quenched

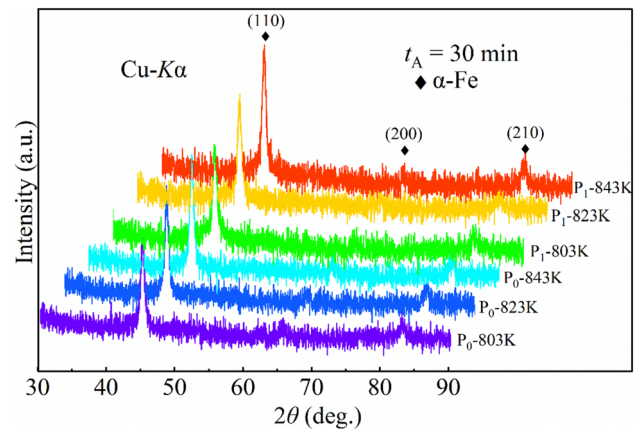


Fig. 3 XRD patterns of P_0 and P_1 at 803, 823, and 843 K

state, (a) and (b), including the curved domains with 180° domain wall and the fingerprint-like maze domains. This domain structure is mainly due to the internal stress induced by fast-quenching, and the narrow maze domains indicate the non-uniformity of the stress [30, 31]. The domain structure of P_0 and P_1 annealed at 843 K contains only 180° linear domains, (c) and (d). This is because the internal stress, magnetocrystalline anisotropy and magnetostriction coefficient of the annealed samples are reduced, resulting in the decrease of effective magnetic anisotropy [27, 32]. Thus, the maze domains disappear, leaving only relatively regular linear domains. In addition, pinning points present in the middle of the domain wall of P_0 . Conversely, P_1 has a wider and better arrangement domain wall than P_0 , which can be attributed to the reduced magnetic crystal anisotropy resulted from its finer and more uniform α -Fe(Si) nanocrystalline grains. This points to a smaller resistance of the magnetic domain movement of P_1 when compared to P_0 ; and a smaller H_c in a wide annealing temperature range.

3.4 Crystallization dynamics analysis

To provide further evidence that trace P addition can effectively refine the grains of the FeSiBCuNb alloy, we performed crystallization thermodynamic analysis via measuring the DSC curves of P_0 and P_1 with heating rates of 5, 10, 20 and 40 K/min. The results are substituted into Kissinger equation [33], and the activation energies. The latter is estimated from the onset of crystallization temperature and the peak temperature, marked as E_{x1} and E_{p1} , respectively. The Kissinger equation is as follows:

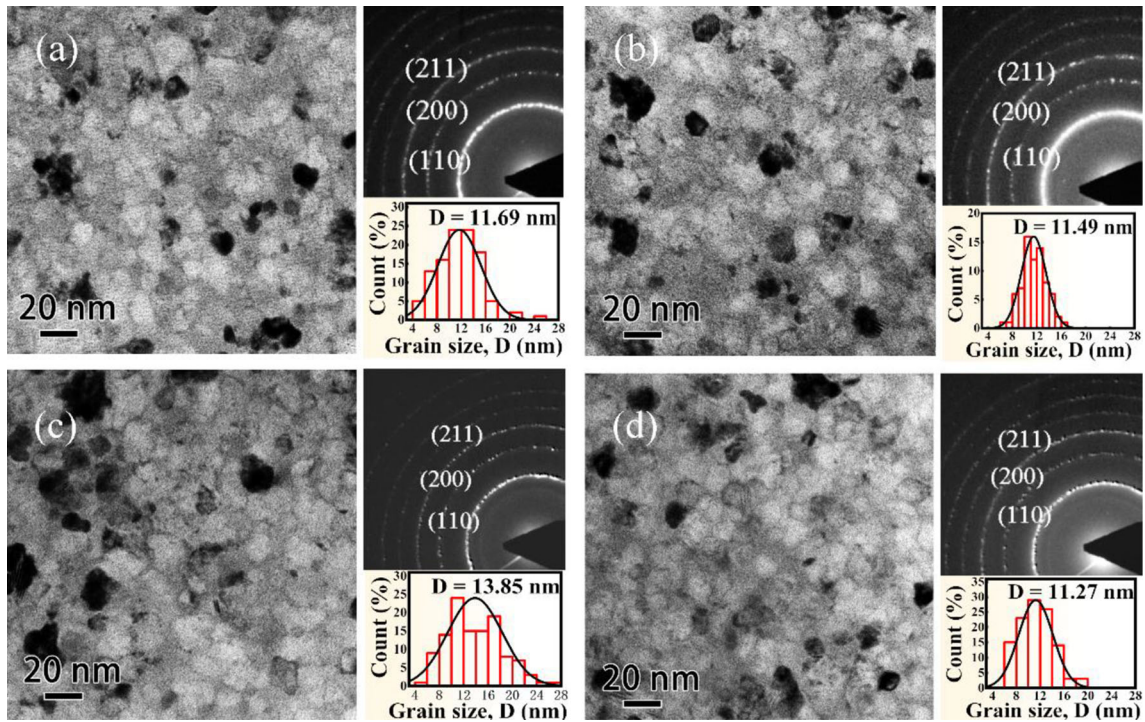
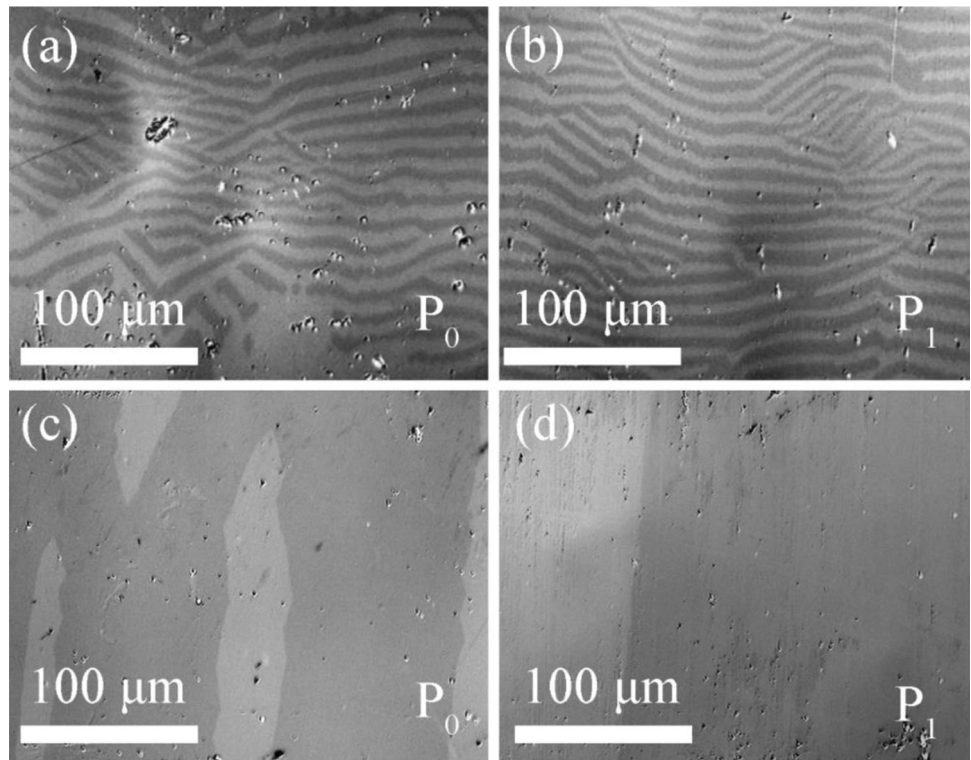


Fig. 4 TEM micrographs, SAED images and characteristic grain size distribution of **a** P₀ at 803 K, **b** P₁ at 803 K, **c** P₀ at 843 K, and **d** P₁ at 843 K

Fig. 5 Magnetic domain structure of P₀ and P₁. **a** and **b** as-quenched; **c** and **d** annealing at 843 K for 30 min



$$\ln\left(\frac{T_p^2}{\beta}\right) = \frac{E_p}{RT_p} + \text{const}, \quad (1)$$

where β is the heating rate, T_p is the crystallization peak temperature at a specific heating rate, R is the perfect gas constant (8.314472 J/mol/K), and E_p is the activation energy of crystallization.

The corresponding Kissinger plot and the specific activation energy of crystallization are shown in Fig. 6. The slope of the fitted curve in Fig. 6a represents the magnitude of the crystallization activation energy. The greater the slope, the greater the activation energy. It can be seen from Fig. 6a that the slope of the fitted curve of P_1 is larger. The E_{x1} values of P_0 and P_1 are greater than the E_{p1} values of P_0 and P_1 (see Fig. 6b), meaning that the nuclear process requires less energy than the growth process. Thus the growth process may occur more frequently than the nucleus process. The E_{x1} and E_{p1} of P_0 are 326 and 308 kJ/mol, respectively. With the addition of 1 at% P, the E_{x1} and E_{p1} of P_1 are increased to 402 kJ/mol and 370 kJ/mol, respectively. Therefore, P_1 requires higher activation energy for nucleation and growth than P_0 , indicating that the nucleation and growth of α -Fe(Si) in P_1 are inhibited effectively. This is consistent with the results of TEM and magneto-optic Kerr microscope.

4 Conclusion

The effect of P microalloying on the magnetic properties and structure of $\text{Fe}_{77.8}\text{Si}_{10}\text{B}_{9-x}\text{Cu}_{0.6}\text{Nb}_{2.6}\text{P}_x$ ($x = 0$ and 1 at%) nanocrystalline alloy has been studied. The substitution of 1 at% P for B has almost no effect on the B_s and μ of the alloy, but the H_c is effectively decreased and stabilized in a wide

annealing temperature range. The analysis of crystallization kinetics shows that the addition of 1 at% P can significantly inhibit the nucleation and growth of crystal grains, thus the P microalloyed alloy can form more uniform and finer α -Fe(Si) grains. This benefits the alloy to obtain low magnetocrystalline anisotropy and wide magnetic domains, and excellent soft magnetic properties, i.e. high B_s of 1.43 T, high μ up to 27,000 at 1 kHz, and low H_c of 1.4 A/m. This work provides a design strategy for low-P nanocrystalline alloys with high AFA and excellent soft magnetic properties.

Author contributions

JL conceived and supervised the study. CW performed the experiments and wrote the first draft. AH and YD improved the manuscript. XZ and JW completed the preliminary experiment.

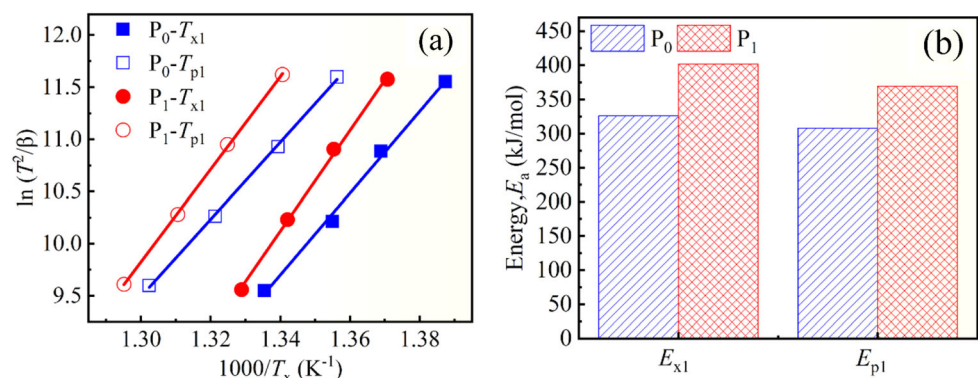
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Compliance with ethical standards

Conflict of interest The authors declare no conflict of interest.

Fig. 6 a Kissinger plots and b crystallization activation energy of P_0 and P_1



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